

Report

Title	Case study 0-1: Introductory (touching trefoil)
Project	Verification CIGRE TB 880
Created	Date: 2025-05-19 Time: 10:57 Software version: 8482 (2025-05-16)

Arrangement

Arrangement	buried project (#46635)
Options	None
CIGRE TB 880, guidance points	02, 06, 26, 31
CIGRE TB 880, test setting	08, 47
Systems	A

Statistics

Number of iterations of the solver	N_{calc}	10
Sum of currents from all systems	I_{sum}	803.16 A
Sum of average conductor temperatures from all systems	θ_{sum}	90 °C
Number of overheated electrical systems		0
Sum of losses from all systems	W_{sum}	105.652 W/m



Systems

Following systems are active in the arrangement:

#	Object	Current [A]	Temp. [°C]	Losses [W/m]	Load
		I_c	$\theta_c \mid \theta_e$	W_{sys}	LF
A	16173 CIGRE TB 880 Case 0 XLPE insulated ca...	803.2	90.0 76.2	105.7	1.00

Objects

Following objects are used:

16173 CIGRE TB 880 Case 0 XLPE insulated cable 132 kV

Ambient

Calculation method		IEC Standard (directly buried)
Ambient temperature	θ_a	20 °C
Thermal resistivity soil	ρ_4	1 K.m/W
Thermal conductivity soil	k_4	1 W/(m.K)
Volumetric heat capacity soil material	$c_{p,soil}$	2136.8 J/(kg.K)
$10^{-4} \frac{k_4^{0.2}}{4.68}$		
Thermal diffusivity soil	δ_{soil}	5.00e-7 m²/s
Ratio thermal resistivity dry/moist soil	v_4	1
$\frac{\rho_{4d}}{\rho_4}$		

Constants

Standard acceleration of gravity	g	9.80665 m/s²
Archimedes' constant π	π	3.141592653589793
Absolute temperature	θ_{abs}	273.15 K
Stefan Boltzmann constant	σ	5.67036713e-8 W/m²K⁴
Vacuum permeability	μ_0	1.2566370614359173e-6 H/m
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m

System A (High voltage cable)**Ampacity**

Cable		CIGRE TB 880 Case 0 XLPE insulated cable 132 kV
Rounded value, CIGRE TB 880	I_c	800 A
Conductor current	I_c	803.16 A
$\sqrt{\frac{\theta_c - \theta_a + (v_4 - 1) \Delta\theta_x - v_4 \Delta\theta_p - \Delta\theta_d}{R_c (T_1 + n_{ph} (1 + \lambda_1) T_2 + (1 + \lambda_1 + \lambda_2 + \lambda_3) (n_{ph} T_3 + n_{cc} (T_{4i} + T_{4ii} + T_{4\mu} v_4)) + n_{cc} \lambda_4 (\frac{T_{4ii}}{2} + T_{4\mu} v_4))}}$		
Operating voltage	U_o	132 kV
Angular frequency $2\pi f$	ω	314.2 rad/s
Number of sources in system	N_c	3
Number of conductors combined	n_{cc}	1

Load

System frequency	f	50 Hz
Continuous load	LF	1 p.u.

Arrangement

Arrangement		trefoil
Position cable 1	$x_1 y_1$	0.0 956.4 mm
Position cable 2	$x_2 y_2$	-37.8 1021.8 mm
Position cable 3	$x_3 y_3$	37.8 1021.8 mm
Separation of conductors in a system	s_c	75.5 mm
Mean distance between the phases	a_m	75.5 mm
Geometric mean distance between phases of the same system S_m	GMD	0.0755 m
Depth of laying of sources	L_c	1000 mm
Depth of laying	L_{cm}	1 m
Outer diameter	D_o	0.0755 m
Substitution coefficient u $\frac{2L_{cm}}{D_o}$	u	26.4901
Geometric constant of circle buried $2u$	g_u	52.9801

Temperature

Temperature conductor $\theta_a + \Delta\theta_c - (v_4 - 1) \Delta\theta_x + v_4 \Delta\theta_p$	θ_c	90 °C
Temperature screen/sheath	θ_s	79.21 °C
Temperature sheath $\theta_c - T_1 \left(W_c + \frac{W_d}{2} \right)$	θ_{sh}	79.21 °C
External temperature object $\theta_c - T_1 \left(W_c + \frac{W_d}{2} \right) - n_{ph} T_2 (W_c (1 + \lambda_1) + W_d) - n_{ph} T_3 (W_I + W_d)$	θ_e	76.16 °C

Temperature rise

Temperature rise conductor	$\Delta\theta_c$	70 K
$n_{ph} (W_c T_{int} + W_d T_d) + n_{cc} \left(W_d (T_{4i} + T_{4ii} + v_4 T_{4ss}) + (W_c + W_s + W_{ar} + W_{sp}) (T_{4i} + T_{4ii} + v_4 T_{4\mu}) + W_{duct} \left(\frac{T_{4ii}}{2} + v_4 T_{4\mu} \right) \right)$		
Temperature rise dielectric losses	$\Delta\theta_d$	0.7284 K
$W_d (n_{ph} T_d + n_{cc} (T_{4i} + T_{4ii} + T_{4ss} v_4))$		
Temperature rise by other buried objects	$\Delta\theta_p$	0 K
$\sum_{k=1}^q \Delta\theta_{kp}$		
Critical soil temperature rise	$\Delta\theta_x$	0 K

Losses**Ohmic**

Conductor losses (phase)	W_c	25.494 W/m
$I_c^2 R_c$		
Screen/sheath losses (phase)	W_s	9.338 W/m
$\lambda_1 W_c$		
Duct losses	W_{duct}	0 W/m
Ohmic losses (phase)	W_I	34.832 W/m
$W_c (1 + \lambda_1 + \lambda_2 + \lambda_3 + \lambda_4)$		

Dielectric

Dielectric losses (phase)	W_d	0.385 W/m
$\omega C_b \left(1000 \frac{U_o}{\sqrt{3}} \right)^2 \tan \delta_i$		

Total

Total losses (phase)	W_t	35.217 W/m
$W_I + W_d$		
Total losses (object)	W_{tot}	35.217 W/m
$n_{ph} W_t$		
Total losses (system)	W_{sys}	105.652 W/m

Thermal resistance

Thermal resistance ambient	$T_{4\mu}$	1.5947 K.m/W
$= T_{4ss} = T_{4iii} = 3 \frac{\rho_4}{2\pi} (\ln(g_u) - 0.63)$		
Thermal resistance jacket	T_3	0.0867 K.m/W
$1.6 T_3$		

Cable

Internal thermal resistance for current losses	T_{int}	0.5384 K.m/W
$\frac{T_1}{n_{ph}} + (1 + \lambda_1) T_2 + (1 + \lambda_1 + \lambda_2 + \lambda_3) T_3$		
Internal thermal resistance for dielectric losses	T_d	0.29666 K.m/W
$\frac{T_1}{2n_c} + T_2 + T_3$		

Other characteristics

Earthing

earthing screen/sheath

both-side bonding

Variation of spacing

No variation

Loss factor

Loss factor shield (screen/sheath)

 λ_1

0.3663

$$\lambda_{11} + F_e \lambda_{12}$$

Loss factor shield, circulating currents

 λ_{11}

0.2935

$$\frac{\frac{R_e}{R_c}}{1 + \left(\frac{R_e}{X_e}\right)^2}$$

Loss factor shield, eddy currents

 λ_{12}

0.0771

$$\frac{R_{sh}}{R_c} \left(g_s \lambda_0 (1 + \Delta_1 + \Delta_2) + \frac{(\beta_1 t_{sh})^4}{12 \cdot 10^{12}} \right)$$

Electrical resistance shield/armour

 R_e 2.0674e-1 Ω /kmSubstitution coefficient λ_0 for eddy-currents λ_0

0.0136

$$3 \frac{m_0^2}{1 + m_0^2} \left(\frac{d_e}{2s_c} \right)^2$$

Substitution coefficient Δ_1 for eddy-currents Δ_1

0.0806

$$(1.14 m_0^{2.45} + 0.33) \left(\frac{d_e}{2s_c} \right)^{0.92 m_0 + 1.66}$$

Substitution coefficient Δ_2 for eddy-currents Δ_2

0

Substitution coefficient m_0 for eddy-currents m_0 0.152 Hz.m/ Ω

$$10^{-7} \frac{\omega}{R_{sh}}$$

Substitution coefficient β_1 for eddy-currents β_1

105.9373

$$\sqrt{\frac{4\pi\omega}{10^7 \rho_{sh} (1 + \alpha_{sh} (\theta_{sh} - 20))}}$$

Substitution coefficient g_s for eddy-currents g_s

1.002454

$$1 + \left(\frac{t_{sh}}{D_{sh}} \right)^{1.74} (10^{-3} \beta_1 D_{sh} - 1.6)$$

Factor F_e eddy-current losses F_e

0.9439

$$\frac{4M_e^2 N_e^2 + (M_e + N_e)^2}{4(M_e^2 + 1)(N_e^2 + 1)}$$

Substitution coefficient M_e to calculate factor F_e M_e

4.1018

$$\frac{R_e}{X_e}$$

Substitution coefficient N_e to calculate factor F_e N_e

4.1018

$$\frac{R_e}{X_e}$$

Loss factor armour

 λ_2

0

Drying-out of soil

Characteristic diameter drying zone

 D_{dry}

0.075 m

Depth characteristic diameter drying zone

 L_{dry}

1 m

Geometric constant of circle drying zone

 g_{dry}

1 p.u.

Substitution coefficient g

 g_a

1

Electrical parameters

System

System length	L_{sys}	1000 m
Power factor	$\cos\varphi$	1

Resistance

Electrical resistance conductor $R_{cDC} (1 + y_s + y_p)$	R_c	$3.9522\text{e-}5 \text{ } \Omega/\text{m} \rightarrow 0.0395 \text{ } \Omega$
Electrical resistance DC conductor $R_{c20} (1 + \alpha_c (\theta_c - 20))$	R_{cDC}	$3.6085\text{e-}5 \text{ } \Omega/\text{m} \rightarrow 0.0361 \text{ } \Omega$
Skin effect factor conductor $\frac{x_s^4}{192 + 0.8x_s^4}$	y_s	0.06012
Factor for skin effect on conductor $\sqrt{10^{-7} \frac{8\pi f}{R_{cDC}} k_s}$	x_s	1.86612
Proximity effect factor conductor $\frac{x_p^4}{192 + 0.8x_p^4} \left(\frac{d_c}{s_c} \right)^2 \left(0.312 \left(\frac{d_c}{s_c} \right)^2 + \frac{1.18}{\frac{x_p^4}{192 + 0.8x_p^4} + 0.27} \right)$	y_p	0.0351
Factor for proximity effect of conductors $\sqrt{10^{-7} \frac{8\pi f}{R_{cDC}} k_p}$	x_p	1.86612
Electrical resistance sheath $R_{sh} (1 + \alpha_{sh} (\theta_{sh} - 20))$	R_{sh}	$2.0674\text{e-}4 \text{ } \Omega/\text{m} \rightarrow 0.2067 \text{ } \Omega$
Electrical resistance shield	R_s	$2.0674\text{e-}4 \text{ } \Omega/\text{m} \rightarrow 0.2067 \text{ } \Omega$
Reduction factor $\frac{R_s}{\sqrt{R_s^2 + X_s^2}}$	RF	0.3064

Electrical field strength, capacitive load current

Electrical field strength insulation inner/outer $\frac{U_e}{1000} \frac{1}{r_x \ln \left(\frac{r_{osc}}{r_{isc}} \right)}$	E_i	$6.956 \mid 3.603 \text{ kV/mm}$
Radius to point x in insulation	r_x	$16.65 \mid 32.15 \text{ mm}$
Line-to-ground voltage $\frac{1000U_o}{\sqrt{3}}$	U_e	76210.24 V
Capacitance insulation $\frac{1}{2\pi\epsilon_0} \frac{10^{-9}}{18} C_b$	C_b	$2.111\text{e-}10 \text{ F/m} \rightarrow 0.2111 \text{ } \mu\text{F}$
Capacitive load current $U_e \omega C_b$	I_C	$5.054\text{e-}3 \text{ A/m} \rightarrow 5.0536 \text{ A}$
Charging capacity $n_{ph} U_e^2 \omega C_b$	P_C	$385.1382 \text{ var/m} \rightarrow 385.1382 \text{ kvar}$
Capacitive earth short-circuit current $U_e \omega C_E$	I_{Ce}	$5.054\text{e-}3 \text{ A/m}$

Reactance

Self reactance conductor X_a 7.088e-4 $\Omega/\text{m} \rightarrow 0.7088 \Omega$

$$\omega \frac{\mu_0}{2\pi} \ln \left(\frac{D_E}{GMR_c} \right)$$

Self reactance screen/sheath X_e 5.040e-5 $\Omega/\text{m} \rightarrow 0.0504 \Omega$

$$\omega \frac{\mu_0}{2\pi} \ln \left(\frac{2s_c}{d_s} \right)$$

Induced current (approximate)

Induced circulating current shield I_s 190.235+0.000j A

$$\max \left(I_c \sqrt{\frac{\lambda_{11, sb} R_c}{R_s}} \right)$$

Loss factor shield, circulating currents $\lambda_{11, sb}$ 0.2935+0.0000j

Load, Voltage drop

Apparent power generator-side S_G 183.627 MVA

$$\sqrt{3} U_o I_c$$

Voltage drop V_{drop} 0.068 V/(A.km) $\rightarrow 55 \text{ V} = 0.04\%$

$$\sqrt{3} (R_c \cos \varphi + \omega L_m \sin \varphi)$$

Inductance (mean) L_m 3.725e-7+0.000e0j H/m $\rightarrow 0.3725 \text{ mH}$

$$\frac{\mu_0}{2\pi} \ln \left(\frac{GMD}{GMR_c} \right)$$

Telegrapher equation

Surge impedance Z_C 42.5858-6.9976j Ω

$$\sqrt{\frac{Z_1}{Y_1}}$$

Propagation constant γ_C 4.640e-7+2.824e-6j

$$\sqrt{Z_1 Y_1}$$

Impedance valid up to 100 Hz without earth return

Positive sequence admittance Y_1 0.000e0+6.631e-8j S/m $\rightarrow 0.0000+0.0001j \text{ S}$

$$G + j\omega C_b$$

Positive sequence impedance Z_1 3.952e-5+1.170e-4j $\Omega/\text{m} \rightarrow 0.0395+0.1170j \Omega$

$$R_1 + jX_1$$

Positive sequence reactance X_1 1.170e-4 $\Omega/\text{m} \rightarrow 0.117 \Omega$

$$\omega \frac{\mu_0}{2\pi} \ln \left(\frac{GMD}{GMR_c} \right)$$

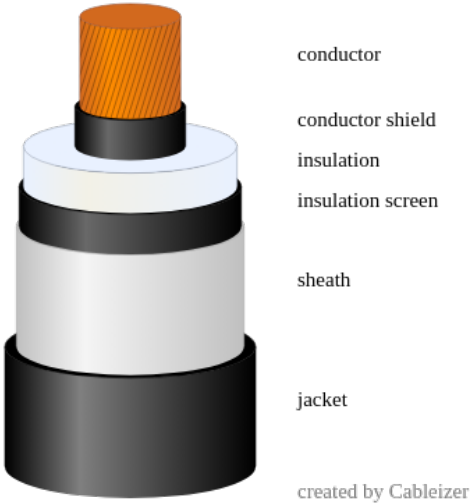
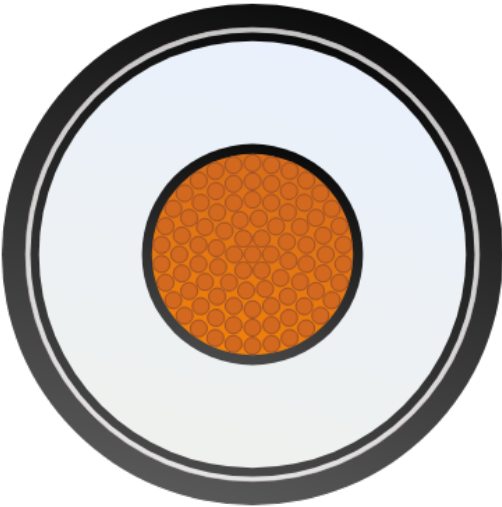
Cable datasheet

TitleCIGRE TB 880 Case 0 XLPE insulated cable 132 kV (#16173)

Cable is used in following systems: [A](#)
CIGRE TB 880, guidance points15, 20, 23, 25, 30, 32, 33, 34, 38, 39, 42, 44, 45

General Data

Rated line-to-line voltage	U_n	132 kV
Base voltage for tests	U_0	76 kV
Highest voltage for equipment	U_m	145 kV
Nominal system frequency	f	50 Hz
Number of conductors cable	n_c	1
Number of phases in a cable	n_{ph}	1



Cable elements

Conductor

Cross-sectional area conductor	A_c	1 x 630 mm ²
Conductor material	M_c	Copper, round stranded
External diameter conductor	d_c	30.3 mm
Radius conductor	r_c	15.15 mm
$\frac{d_c}{2}$		

Insulation

Insulation material	M_i	Crosslinked polyethylene (XLPE)
Thickness conductor shield	t_{cs}	1.5 mm
Thickness insulation	t_{ins}	15.5 mm
Thickness insulation screen	t_{is}	1.3 mm
Thickness insulation	t_i	18.3 mm
$t_{ct} + t_{cs} + t_{ins} + t_{is}$		

Sheath

Sheath material	M_{sh}	Aluminium
Thickness sheath	t_{sh}	0.8 mm
corrugated		No

Jacket

Jacket material	M_j	High density polyethylene (HDPE, ST7)
Thickness jacket	t_j	3.5 mm

Overall

External diameter object	D_e	75.5 mm
Absorption coefficient solar radiation	σ_{sun}	0.4
Emissivity cable	ϵ_e	0.9
Reflectivity cable	η_e	0.1
$1 - \epsilon_e$		
Mass cable	m_{tot}	9.418 kg/m
$m_{hollow} + m_{metal}$		

Electrical**Conductor**

Electrical resistance DC conductor 20°C	R_{c20}	2.8300e-5 Ω /m
Standard DC resistance of conductor	R_{co}	0.0283 Ω /km
Coating of wires		plain
Skin effect coefficient	k_s	1
Proximity effect coefficient	k_p	1
Geometric mean radius conductor	GMR_c	0.01173 m
$K_{GMR} r_{z1}$		
Factor geometric mean radius	K_{GMR}	0.774
Constant relating to conductor formation	K_{BICC}	0.0512
Number of wires conductor	n_{cw}	91
Diameter of wires conductor (average)	d_{cw}	2.97 mm

Insulation

Capacitance, with approximation (CIGRE TB 880)	C_b	2.111e-10 F/m
$\frac{1}{2\pi\epsilon_0} \frac{10^{-9}}{18} C_b$		
Capacitance (exact)	C_b	2.114e-10 F/m
$\frac{2\pi\epsilon_0\epsilon_i}{\ln\left(\frac{r_{osc}}{r_{isc}}\right)}$		
Capacitance to earth	C_E	2.111e-10 F/m
C_b		
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m
Radius above the inner semi-conducting layer	r_{isc}	16.65 mm
$\frac{d_c}{2} + t_{ct} + t_{cs}$		
Radius over capacitive insulation layers	r_{osc}	32.15 mm
$\frac{D_{ins}}{2}$		

Velocity of propagation	v_{prop}	189605.4 km/s
$\frac{1}{1000\sqrt{\mu_0\epsilon_0\epsilon_i}}$		

Screen + Sheath

Electrical resistance sheath	R_{sh}	1.6691e-4 Ω /m
$10^6 \frac{\rho_{sh}}{A_{sh}}$		
Electrical resistance screen/sheath 20°C	R_{so}	1.669e-1 Ω /km

Radius

Radius conductor	r_{z1}	0.01515 m
Radius shield (inner)	r_{z2}	0.03305 m
Radius shield (outer)	r_{z3}	0.03305 m
Radius sheath (inner)	$r_{z2,sh}$	0.03305 m
Radius sheath (outer)	$r_{z3,sh}$	0.03465 m
Radius outersheath	r_{z6}	0.03775 m

Material parameters

Conductor

Electrical resistivity conductor material	ρ_c	1.724e-8 Ω .m
Temperature coefficient conductor material	α_c	3.93e-3 1/K
Reciprocal of temperature coefficient conductor material	β_c	2.345e2 K
Volumetric heat capacity conductor material	σ_c	3.45e6 J/(K.m ³)
Thermal conductivity conductor material	k_c	384.62 W/(m.K)
Density conductor material	ζ_c	8.94 g/cm ³

Insulation

Relative permittivity insulation material	ϵ_i	2.5
Loss factor insulation material	$\tan\delta_i$	0.001
Thermal resistivity insulation material	ρ_i	3.5 K.m/W
Volumetric heat capacity insulation material	σ_i	2.40e6 J/(K.m ³)
Density insulation material	ζ_i	0.923 g/cm ³
Max. temperature conductor	θ_{cmax}	90 °C
Max. temperature conductor, emergency overload	θ_{cmaxeo}	105 °C
Max. temperature conductor, short-circuit	θ_{cmaxsc}	250 °C

Conductor shield

Thermal resistivity conductor shield	ρ_{cs}	2.5 K.m/W
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Insulation screen

Thermal resistivity insulation screen	ρ_{is}	2.5 K.m/W
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Sheath

Specific electrical resistivity sheath material	ρ_{sh}	2.840e-8 Ω .m
Temperature coefficient sheath material	α_{sh}	4.03e-3 1/K
Reciprocal of temperature coefficient sheath material	β_{sh}	2.281e2 K
Volumetric heat capacity sheath material	σ_{sh}	2.50e6 J/(K.m ³)
Thermal conductivity sheath material	k_{sh}	208.3 W/(m.K)
Density sheath material	ζ_{sh}	2.712 g/cm ³

Jacket

Thermal resistivity jacket material	ρ_j	3.5 K.m/W
Thermal resistivity additional layer	ρ_{jj}	2.5 K.m/W
Volumetric heat capacity jacket material	σ_j	2.40e6 J/(K.m ³)
Electrical conductivity jacket material	κ_j	2.00e-15 S/m
Density jacket material	ζ_j	0.941 g/cm ³

Thermal resistance**Internal thermal resistances for rating calculation**

Thermal resistance conductor—sheath $T_{ct} + T_{cs} + T_{ins} + T_{is} + T_{scb} + T_{scs} + T_{dsh}$	T_1	0.4199 K.m/W
Thermal resistance armour bedding	T_2	0 K.m/W
Thermal resistance jacket $T_{ab} + T_j + T_{jj}$	T_3	0.0542 K.m/W
Thickness conductor—sheath $t_i + t_{scb} + t_{scs} + \frac{H_{sh} + \Delta H}{2}$	t_1	18.3 mm
Thickness sheath—armour $\frac{H_{sh} + \Delta H}{2} + t_{ab}$	t_2	0 mm
Thickness armour—surface $t_j + t_{jj}$	t_3	3.5 mm

Cable elements

Thermal resistance, transient $T_1 + T_2 + T_3$	T_{tot}	0.4741 K.m/W
Thermal resistance insulation $T_{ct} + T_{cs} + T_{ins} + T_{is}$	T_i	0.41987 K.m/W
Thermal resistance conductor shield $\frac{\rho_{cs}}{2\pi} \ln \left(\frac{D_{cs}}{D_{cs} - 2t_{cs}} \right)$	T_{cs}	0.03756 K.m/W
Thermal resistance insulation $\frac{\rho_i}{2\pi} \ln \left(\frac{D_{ins}}{D_{ins} - 2t_{ins}} \right)$	T_{ins}	0.36654 K.m/W
Thermal resistance insulation screen $\frac{\rho_{is}}{2\pi} \ln \left(\frac{D_{ins} + 2t_{is}}{D_{ins}} \right)$	T_{is}	0.01577 K.m/W
Thermal resistance jacket $\frac{\rho_j}{2\pi} \ln \left(\frac{D_j - 2t_{jj}}{D_j - 2(t_j + t_{jj})} \right)$	T_j	0.0542 K.m/W

Dimensions**Diameter**

External diameter conductor	d_c	30.3 mm
Diameter over conductor shield $d_c + 2(t_{ct} + t_{cs})$	D_{cs}	33.3 mm
Diameter over insulation $d_c + 2(t_{ct} + t_{cs} + t_{ins})$	D_{ins}	64.3 mm

Diameter over insulation incl. insulation screen $d_c + 2(t_{ct} + t_{cs} + t_{ins} + t_{is})$	D_i	66.9 mm
Diameter over insulation screen $d_c + 2t_i$	D_{is}	66.9 mm
Equivalent diameter of screen and sheath	d_s	67.7 mm
Mean diameter sheath $D_{shb} + t_{sh} + H_{sh} + \Delta H$	d_{sh}	67.7 mm
Diameter over sheath $D_{shb} + 2(t_{sh} + H_{sh} + \Delta H)$	D_{sh}	68.5 mm
Diameter over sheath jacket	D_{shj}	68.5 mm
Diameter over jacket $D_{ar} + 2(t_j + t_{jj})$	D_j	75.5 mm

Area

Cross-sectional area conductor	A_c	630 mm ²
Cross-sectional area insulation $\frac{\pi}{4}(D_{is}^2 - d_c^2)$	A_i	2794.1 mm ²
Cross-sectional area sheath $d_{sh}t_{sh}\pi$	A_{sh}	170.15 mm ²
Cross-sectional area jacket $\frac{\pi}{4}(D_j^2 - (D_j - 2(t_j + t_{jj}))^2)$	A_j	791.7 mm ²