

Report

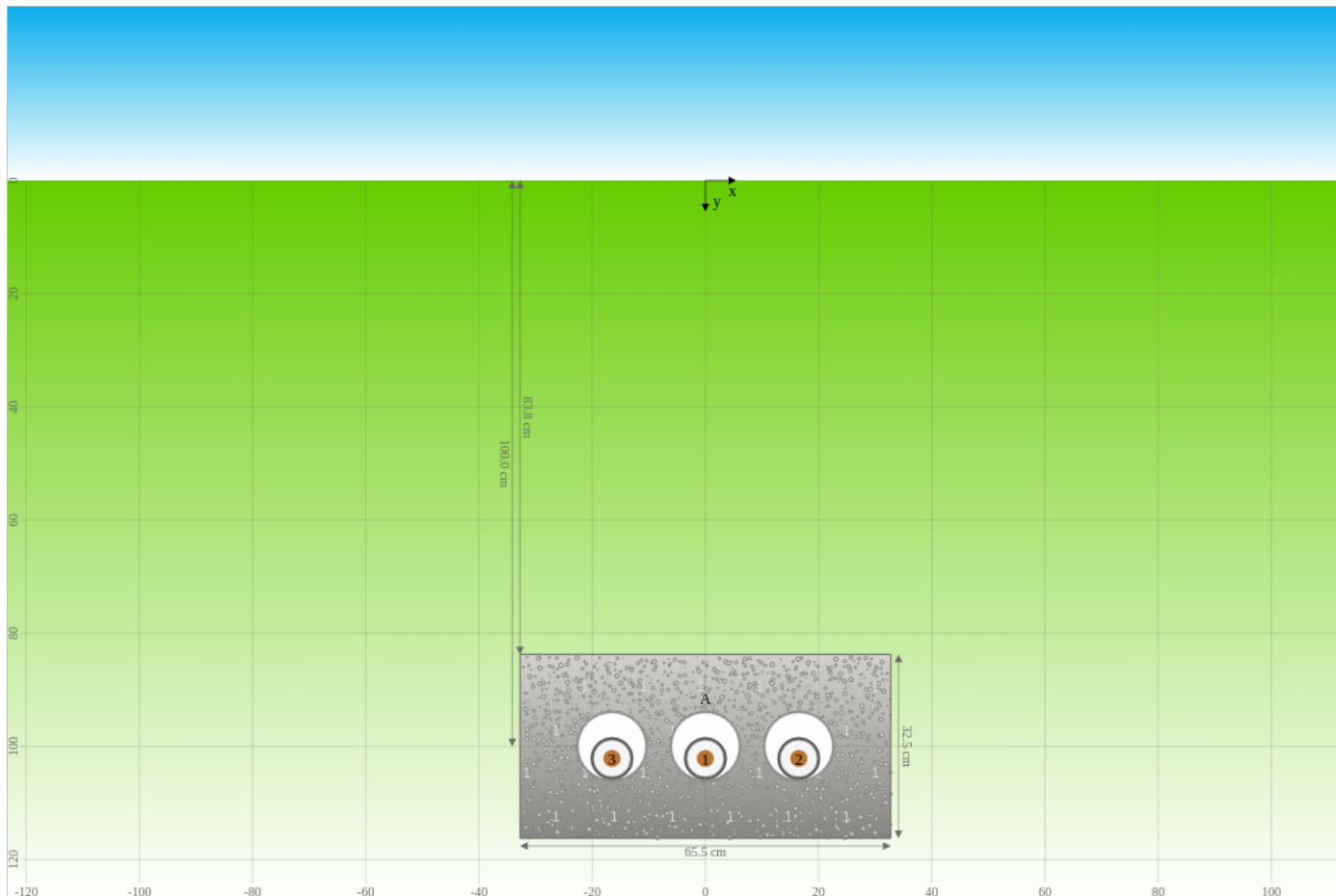
Title	Case study 0-3: Introductory (ductbank)
Project	Verification CIGRE TB 880
Created	Date: 2025-05-14 Time: 21:40 Software version: 51cac (2025-05-14)

Arrangement

Arrangement	buried project (#46691)
Options	None
CIGRE TB 880, guidance points	02, 06, 26, 31
Systems	A

Statistics

Number of iterations of the solver	N_{calc}	31
Sum of currents from all systems	I_{sum}	633.45 A
Sum of average conductor temperatures from all systems	θ_{sum}	85.01 °C
Number of overheated electrical systems		0
Sum of losses from all systems	W_{sum}	104.714 W/m



Systems

Following systems are active in the arrangement:

#	Object	Current [A] I_c	Temp. [°C] $\theta_c \mid \theta_e \ (\theta_{de})$	Losses [W/m] W_{sys}	Load LF
A	16173 CIGRE TB 880 Case 0 XLPE insulated ca...	633.4	90.0 81.1 (64.4)	104.7	1.00

Objects

Following objects are used:

16173 CIGRE TB 880 Case 0 XLPE insulated cable 132 kV

Ambient

Calculation method		IEC Standard (with backfill)
Ambient temperature	θ_a	20 °C
Thermal resistivity soil	ρ_4	1 K.m/W
Thermal conductivity soil	k_4	1 W/(m.K)
Volumetric heat capacity soil material	$c_{p,soil}$	2136.8 J/(kg.K)
$10^{-4} \frac{k_4^{0.2}}{4.68}$		
Thermal diffusivity soil	δ_{soil}	5.00e-7 m ² /s
Ratio thermal resistivity dry/moist soil	v_4	1
$\frac{\rho_{4d}}{\rho_4}$		

Constants

Standard acceleration of gravity	g	9.80665 m/s ²
Archimedes' constant π	π	3.141592653589793
Absolute temperature	θ_{abs}	273.15 K
Stefan Boltzmann constant	σ	5.67036713e-8 W/m ² K ⁴
Vacuum permeability	μ_0	1.2566370614359173e-6 H/m
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m

Zones

Backfill 1

Calculation method		IEC 60287-2-1 ed2.0 (2015)
Thermal resistivity backfill	ρ_b	0.8 K.m/W
Horizontal center backfill	x_b	0 mm
Vertical center backfill	L_b	1000 mm
Height backfill	h_b	325 mm
Width backfill	w_b	655 mm
Geometric factor backfill	G_b	2.185
$\ln(u_b + \sqrt{u_b^2 - 1})$		
Substitution coefficient u	u_b	4.502
$\frac{L_b}{r_b}$		
Equivalent radius backfill	r_b	222.1 mm
$e^{\frac{\text{Min}(w_b, h_b)}{2 \text{Max}(w_b, h_b)} \left(\frac{4}{\pi} - \frac{\text{Min}(w_b, h_b)}{\text{Max}(w_b, h_b)} \right) \ln \left(1 + \left(\frac{\text{Max}(w_b, h_b)}{\text{Min}(w_b, h_b)} \right)^2 \right) + \ln \left(\frac{\text{Min}(w_b, h_b)}{2} \right)}$		

System A (High voltage cable)

Ampacity

Cable		CIGRE TB 880 Case 0 XLPE insulated cable 132 kV
Rounded value, CIGRE TB 880	I_c	630 A
Conductor current	I_c	633.45 A
$\sqrt{\frac{\theta_c - \theta_a + (v_4 - 1) \Delta\theta_x - v_4 \Delta\theta_p - \Delta\theta_d}{R_c (T_1 + n_{ph} (1 + \lambda_1) T_2 + (1 + \lambda_1 + \lambda_2 + \lambda_3) (n_{ph} T_3 + n_{cc} (T_{4i} + T_{4ii} + T_{4\mu} v_4)) + n_{cc} \lambda_4 \left(\frac{T_{4ii}}{2} + T_{4\mu} v_4 \right)}}$		
Operating voltage	U_o	132 kV
Angular frequency $2\pi f$	ω	314.2 rad/s
Number of sources in system	N_c	3
Number of conductors combined	n_{cc}	1

Load

System frequency	f	50 Hz
Continuous load	LF	1 p.u.

Arrangement

Duct material	M_d	duct made of plastic PVC (polyvinylchloride)
Diameter duct inner, outer	$Di_d Do_d$	118.6 125.0 mm
Thermal resistivity duct material	ρ_d	6 K.m/W
Volumetric heat capacity duct material	σ_d	1.70e6 J/(K.m ³)
Absorption coefficient solar radiation	σ_{sun}	0.6
Arrangement		flat
Position duct 1	$x_1 y_1$	0.0 1000.0 mm
Position duct 2	$x_2 y_2$	165.0 1000.0 mm
Position duct 3	$x_3 y_3$	-165.0 1000.0 mm
Separation of conductors in a system	s_c	165 mm
Mean distance between the phases	a_m	207.89 mm
Geometric mean distance between phases of the same system $2^{\frac{1}{3}} S_m$	GMD	0.20789 m
Depth of laying of sources	L_c	1000 mm
Depth of laying	L_{cm}	1 m
Outer diameter	Do	0.125 m
Substitution coefficient u $\frac{2L_{cm}}{Do}$	u	16
Geometric constant of circle buried $u + \sqrt{u^2 - 1}$	g_u	31.9687

Temperature

Temperature conductor $\theta_a + \Delta\theta_c - (v_4 - 1) \Delta\theta_x + v_4 \Delta\theta_p$	θ_c	1: 81.44 2: 83.58 3: 90 °C
Temperature screen/sheath	θ_s	1: 75.02 2: 77.12 3: 83.43 °C
Temperature sheath $\theta_c - T_1 \left(W_c + \frac{W_d}{2} \right)$	θ_{sh}	1: 75.02 2: 77.12 3: 83.43 °C

External temperature object θ_e 1: 73.54 | 2: 75.23 | 3: 81.13 °C

$$\theta_e - T_1 \left(W_c + \frac{W_d}{2} \right) - n_{ph} T_2 (W_c (1 + \lambda_1) + W_d) - n_{ph} T_3 (W_I + W_d)$$

Duct

Mean temperature medium in the duct θ_{dm} 1: 68.67 | 2: 69.07 | 3: 73.81 °C

$$\frac{\theta_e}{2} + \frac{\theta_{di}}{2}$$

Temperature duct inner surface θ_{di} 1: 63.8 | 2: 62.92 | 3: 66.48 °C

$$\theta_e - T_{4i} n_{cc} (W_I + W_d)$$

Temperature duct outer surface θ_{de} 1: 62.42 | 2: 61.17 | 3: 64.35 °C

$$\theta_{di} - T_{4ii} n_{cc} W_t + \frac{T_{4ii} W_{duct}}{2} n_{cc}$$

Temperature rise

Temperature rise conductor $\Delta\theta_c$ 1: 36.8726 | 2: 45.035 | 3: 53.2164 K

$$n_{ph} (W_c T_{int} + W_d T_d) + n_{cc} \left(W_d (T_{4i} + T_{4ii} + v_4 T_{4ss}) + (W_c + W_s + W_{ar} + W_{sp}) (T_{4i} + T_{4ii} + v_4 T_{4\mu}) + W_{duct} \left(\frac{T_{4ii}}{2} + v_4 T_{4\mu} \right) \right)$$

Temperature rise dielectric losses $\Delta\theta_d$ 1: 0.5079 | 2: 0.5076 | 3: 0.5043 K

$$W_d (n_{ph} T_d + n_{cc} (T_{4i} + T_{4ii} + T_{4ss} v_4))$$

Temperature rise duct (magnetic) $\Delta\theta_{duct}$ 0 K

Temperature rise by other buried objects $\Delta\theta_p$ 1: 24.5718 | 2: 18.5434 | 3: 16.7838 K

$$\sum_{k=1}^q \Delta\theta_{kp}$$

Critical soil temperature rise $\Delta\theta_x$ 0 K

Losses

Ohmic

Conductor losses (phase) W_c 1: 15.096 | 2: 15.186 | 3: 15.455 W/m

$$I_c^2 R_c$$

Screen/sheath losses (phase) W_s 1: 11.984 | 2: 19.247 | 3: 26.59 W/m

$$\lambda_1 W_c$$

Duct losses W_{duct} 0 W/m

Ohmic losses (phase) W_I 1: 27.081 | 2: 34.432 | 3: 42.045 W/m

$$W_c (1 + \lambda_1 + \lambda_2 + \lambda_3 + \lambda_4)$$

Dielectric

Dielectric losses (phase) W_d 0.385 W/m

$$\omega C_b \left(1000 \frac{U_o}{\sqrt{3}} \right)^2 \tan \delta_i$$

Total

Total losses (phase) W_t 1: 27.466 | 2: 34.818 | 3: 42.43 W/m

$$W_I + W_d$$

Total losses (object) W_{tot} 1: 27.466 | 2: 34.818 | 3: 42.43 W/m

$$n_{ph} W_t$$

Total losses (system) W_{sys} 104.714 W/m

Thermal resistance

Thermal resistance ambient $T_{4\mu}$ 0.6498 K.m/W
 $= T_{4ss} = T_{4iii} + T_{4db}$

Thermal resistance ambient T_{4iii} 0.4411 K.m/W
 $\frac{\rho_4}{2\pi} (\ln(g_u) + \ln(F_{mh}))$

Mutual heating coefficient F_{mh} 1

Backfill

Thermal resistance backfill correction T_{4db} 0.2087 K.m/W
 $\frac{N_b (\rho_4 - \rho_b)}{2\pi} G_b$

Number of loaded objects in backfill N_b 3

Duct

Thermal resistance medium in the duct T_{4i} 1: 0.3546 | 2: 0.3538 | 3: 0.3452 K.m/W
 $\frac{U_d}{1 + 0.1 (V_d + Y_d \theta_{dm}) D_{eq}}$

Constant U for cables in ducts U_d 1.87

Constant V for cables in ducts V_d 0.312

Constant Y for cables in ducts Y_d 0.0037

Thermal resistance duct wall T_{4ii} 0.0502 K.m/W
 $\frac{\rho_d}{2\pi} \ln \left(\frac{D_{od}}{D_{id}} \right)$

Cable

Internal thermal resistance for current losses T_{int} 1: 0.5171 | 2: 0.5428 | 3: 0.5673 K.m/W
 $\frac{T_1}{n_{ph}} + (1 + \lambda_1) T_2 + (1 + \lambda_1 + \lambda_2 + \lambda_3) T_3$

Internal thermal resistance for dielectric losses T_d 0.26414 K.m/W
 $\frac{T_1}{2n_c} + T_2 + T_3$

Other characteristics**Earthing**

earthing screen/sheath both-side bonding
 Variation of spacing No variation

Loss factor

Loss factor shield (screen/sheath) λ_1 1: 0.7939 | 2: 1.2674 | 3: 1.7204
 $\lambda_{11} + \lambda_{12}$

Loss factor shield, circulating currents λ_{11} 1: 0.7939 | 2: 1.2674 | 3: 1.7204
 $\frac{R_e}{R_c} 4\xi_{X,2}$

$$\frac{R_e}{R_c} (\xi_{X,3} + \xi_{X,2} - \xi_{X,1})$$

$$\frac{R_e}{R_c} (\xi_{X,3} + \xi_{X,2} + \xi_{X,1})$$

Parameter ξ calculation of loss factor	ξ_X	1: 0.0412 2: 0.0366 3: 0.2384
$\frac{2R_e P_X Q_X X_m}{\sqrt{3} (R_e^2 + P_X^2) (R_e^2 + Q_X^2)}$		
$\frac{0.25 Q_X^2}{R_e^2 + Q_X^2}$		
$\frac{0.75 P_X^2}{R_e^2 + P_X^2}$		
Loss factor shield, eddy currents	λ_{12}	0
Electrical resistance shield/armour	R_e	1: 2.0393e-1 2: 2.0534e-1 3: 2.0958e-1 Ω/km
Factor F_e eddy-current losses	F_e	1
Loss factor armour	λ_2	0

Drying-out of soil

Characteristic diameter drying zone	D_{dry}	0.125 m
Depth characteristic diameter drying zone	L_{dry}	1 m
Geometric constant of circle drying zone	g_{dry}	1 p.u.
Substitution coefficient g	g_a	1

Electrical parameters

System

System length	L_{sys}	1000 m
Power factor	$\cos\varphi$	1

Resistance

Electrical resistance conductor $R_{cDC} (1 + y_s + y_p)$	R_c	1: 3.7622e-5 2: 3.7845e-5 3: 3.8517e-5 Ω/m
Electrical resistance DC conductor $R_{c20} (1 + \alpha_c (\theta_c - 20))$	R_{cDC}	1: 3.5134e-5 2: 3.5371e-5 3: 3.6085e-5 Ω/m
Skin effect factor conductor $\frac{x_s^4}{192 + 0.8x_s^4}$	y_s	1: 0.06326 2: 0.06245 3: 0.06012
Factor for skin effect on conductor $\sqrt{10^{-7} \frac{8\pi f}{R_{cDC}} k_s}$	x_s	1: 1.89122 2: 1.88487 3: 1.86612
Proximity effect factor conductor $\frac{x_p^4}{192 + 0.8x_p^4} \left(\frac{d_c}{s_c} \right)^2 \left(0.312 \left(\frac{d_c}{s_c} \right)^2 + \frac{1.18}{\frac{x_p^4}{192 + 0.8x_p^4} + 0.27} \right)$	y_p	1: 0.00758 2: 0.0075 3: 0.00727
Factor for proximity effect of conductors $\sqrt{10^{-7} \frac{8\pi f}{R_{cDC}} k_p}$	x_p	1: 1.89122 2: 1.88487 3: 1.86612
Electrical resistance sheath $R_{sh} (1 + \alpha_{sh} (\theta_{sh} - 20))$	R_{sh}	1: 2.0393e-4 2: 2.0534e-4 3: 2.0958e-4 Ω/m
Electrical resistance shield	R_s	1: 2.0393e-4 2: 2.0534e-4 3: 2.0958e-4 Ω/m
Reduction factor $\frac{R_s}{\sqrt{R_s^2 + X_s^2}}$	RF	1: 0.3026 2: 0.3045 3: 0.3102

Electrical field strength, capacitive load current

Electrical field strength insulation inner/outer $\frac{U_e}{1000} \frac{1}{r_x \ln \left(\frac{r_{osc}}{r_{isc}} \right)}$	E_i	6.956 3.603 kV/mm
Radius to point x in insulation	r_x	16.65 32.15 mm
Line-to-ground voltage $\frac{1000U_o}{\sqrt{3}}$	U_e	76210.24 V
Capacitance insulation $\frac{1}{2\pi\epsilon_0} \frac{10^{-9}}{18} C_b$	C_b	2.111e-10 F/m $\rightarrow$ 0.2111 μ F
Capacitive load current $U_e \omega C_b$	I_C	5.054e-3 A/m $\rightarrow$ 5.0536 A
Charging capacity $n_{ph} U_e^2 \omega C_b$	P_C	385.1382 var/m $\rightarrow$ 385.1382 kvar
Capacitive earth short-circuit current $U_e \omega C_E$	I_{Ce}	5.054e-3 A/m

Reactance

Self reactance conductor $\omega \frac{\mu_0}{2\pi} \ln \left(\frac{D_E}{GMR_c} \right)$	X_a	7.088e-4 Ω /m $\rightarrow$ 0.7088 Ω
Self reactance screen/sheath $\omega \frac{\mu_0}{2\pi} \ln \left(\frac{2s_c}{d_s} \right)$	X_e	9.953e-5 Ω /m $\rightarrow$ 0.0995 Ω
Mutual reactance between conductors flat formation without transposition $\omega \frac{\mu_0}{2\pi} \ln 2$	X_m	4.355e-5 Ω /m
Substitution coefficient P to calculate loss factor by circulating currents $X_e + X_m$	P_X	1.431e-4
Substitution coefficient Q to calculate loss factor by circulating currents $X_e - \frac{X_m}{3}$	Q_X	8.501e-5

Induced current (approximate)

Induced circulating current shield $\max \left(I_c \sqrt{\frac{\lambda_{11, sb} R_c}{R_s}} \right)$	I_s	356.190+0.000j A
Loss factor shield, circulating currents	$\lambda_{11, sb}$	1: 0.7939+0.0000j 2: 1.2674+0.0000j 3: 1.7204+0.0000j

Load, Voltage drop

Apparent power generator-side $\sqrt{3} U_o I_c$	S_G	144.826 MVA
Voltage drop $\sqrt{3} (R_c \cos \varphi + \omega L_m \sin \varphi)$	V_{drop}	0.065 V/(A.km) $\rightarrow$ 41.3 V = 0.03%

Inductance (mean) $\frac{\mu_0}{2\pi} \ln \left(\frac{GMD}{GMR_c} \right)$	L_m	5.750e-7+0.000e0j H/m → 0.575 mH
Telegrapher equation		
Surge impedance $\sqrt{\frac{Z_1}{Y_1}}$	Z_C	1: 52.4740-5.4061j 2: 52.4773-5.4378j 3: 52.4873-5.5333j Ω
Propagation constant $\sqrt{Z_1 Y_1}$	γ_C	1: 3.585e-7+3.480e-6j 2: 3.606e-7+3.480e-6j 3: 3.669e-7+3.481e-6j
Impedance valid up to 100 Hz without earth return		
Positive sequence admittance $G + j\omega C_b$	Y_1	0.000e0+6.631e-8j S/m → 0.0000+0.0001j S
Positive sequence impedance $R_1 + jX_1$	Z_1	1: 3.762e-5+1.807e-4j 2: 3.785e-5+1.807e-4j 3: 3.852e-5+1.807e-4j Ω/m
Positive sequence reactance $\omega \frac{\mu_0}{2\pi} \ln \left(\frac{GMD}{GMR_c} \right)$	X_1	1.807e-4 Ω/m → 0.1807 Ω

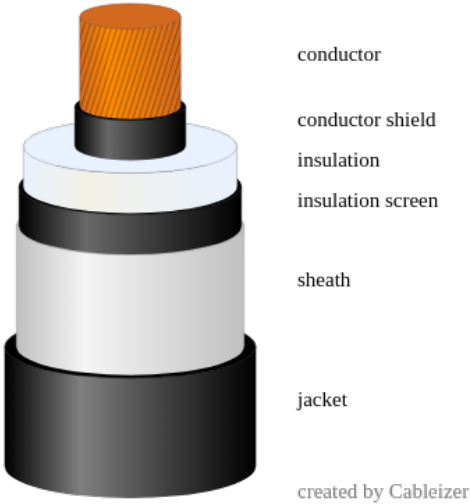
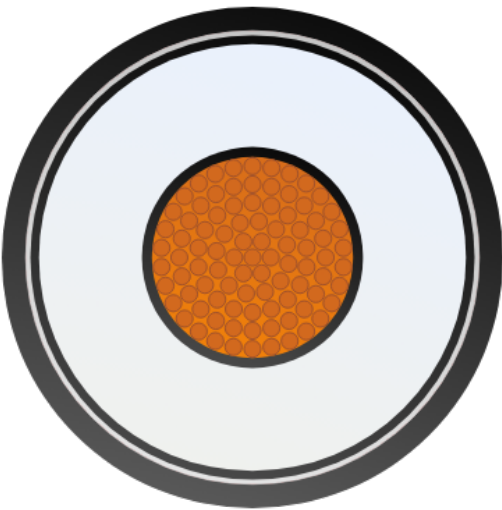
Cable datasheet

TitleCIGRE TB 880 Case 0 XLPE insulated cable 132 kV (#16173)

Cable is used in following systems: [A](#)
CIGRE TB 880, guidance points15, 20, 23, 25, 30, 32, 33, 34, 38, 39, 42, 44, 45

General Data

Rated line-to-line voltage	U_n	132 kV
Base voltage for tests	U_0	76 kV
Highest voltage for equipment	U_m	145 kV
Nominal system frequency	f	50 Hz
Number of conductors cable	n_c	1
Number of phases in a cable	n_{ph}	1



Cable elements

Conductor

Cross-sectional area conductor	A_c	1 x 630 mm ²
Conductor material	M_c	Copper, round stranded
External diameter conductor	d_c	30.3 mm
Radius conductor	r_c	15.15 mm
$\frac{d_c}{2}$		

Insulation

Insulation material	M_i	Crosslinked polyethylene (XLPE)
Thickness conductor shield	t_{cs}	1.5 mm
Thickness insulation	t_{ins}	15.5 mm
Thickness insulation screen	t_{is}	1.3 mm
Thickness insulation	t_i	18.3 mm
$t_{ct} + t_{cs} + t_{ins} + t_{is}$		

Sheath

Sheath material	M_{sh}	Aluminium
Thickness sheath corrugated	t_{sh}	0.8 mm No

Jacket

Jacket material	M_j	High density polyethylene (HDPE, ST7)
Thickness jacket	t_j	3.5 mm

Overall

External diameter object	D_e	75.5 mm
Absorption coefficient solar radiation	σ_{sun}	0.4
Emissivity cable	ϵ_e	0.9
Reflectivity cable $1 - \epsilon_e$	η_e	0.1
Mass cable $m_{hollow} + m_{metal}$	m_{tot}	9.418 kg/m

Electrical**Conductor**

Electrical resistance DC conductor 20°C	R_{c20}	2.8300e-5 Ω /m
Standard DC resistance of conductor	R_{co}	0.0283 Ω /km
Coating of wires		plain
Skin effect coefficient	k_s	1
Proximity effect coefficient	k_p	1
Geometric mean radius conductor $K_{GMR} r_{z1}$	GMR_c	0.01173 m
Factor geometric mean radius	K_{GMR}	0.774
Constant relating to conductor formation	K_{BICC}	0.0512
Number of wires conductor	n_{cw}	91
Diameter of wires conductor (average)	d_{cw}	2.97 mm

Insulation

Capacitance, with approximation (CIGRE TB 880) $\frac{1}{2\pi\epsilon_0} \frac{10^{-9}}{18} C_b$	C_b	2.111e-10 F/m
Capacitance (exact) $\frac{2\pi\epsilon_0\epsilon_i}{\ln\left(\frac{r_{osc}}{r_{isc}}\right)}$	C_b	2.114e-10 F/m
Capacitance to earth C_b	C_E	2.111e-10 F/m
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m
Radius above the inner semi-conducting layer $\frac{d_c}{2} + t_{ct} + t_{cs}$	r_{isc}	16.65 mm
Radius over capacitive insulation layers $\frac{D_{ins}}{2}$	r_{osc}	32.15 mm

Velocity of propagation $\frac{1}{1000\sqrt{\mu_0\epsilon_0\epsilon_i}}$	v_{prop}	189605.4 km/s
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Screen + Sheath

Electrical resistance sheath $10^6 \frac{\rho_{sh}}{A_{sh}}$	R_{sh}	1.6691e-4 Ω /m
Electrical resistance screen/sheath 20°C	R_{so}	1.669e-1 Ω /km

Radius

Radius conductor	r_{z1}	0.01515 m
Radius shield (inner)	r_{z2}	0.03305 m
Radius shield (outer)	r_{z3}	0.03305 m
Radius sheath (inner)	$r_{z2,sh}$	0.03305 m
Radius sheath (outer)	$r_{z3,sh}$	0.03465 m
Radius outersheath	r_{z6}	0.03775 m

Material parameters

Conductor

Electrical resistivity conductor material	ρ_c	1.724e-8 Ω .m
Temperature coefficient conductor material	α_c	3.93e-3 1/K
Reciprocal of temperature coefficient conductor material	β_c	2.345e2 K
Volumetric heat capacity conductor material	σ_c	3.45e6 J/(K.m ³)
Thermal conductivity conductor material	k_c	384.62 W/(m.K)
Density conductor material	ζ_c	8.94 g/cm ³

Insulation

Relative permittivity insulation material	ϵ_i	2.5
Loss factor insulation material	$\tan\delta_i$	0.001
Thermal resistivity insulation material	ρ_i	3.5 K.m/W
Volumetric heat capacity insulation material	σ_i	2.40e6 J/(K.m ³)
Density insulation material	ζ_i	0.923 g/cm ³
Max. temperature conductor	θ_{cmax}	90 °C
Max. temperature conductor, emergency overload	θ_{cmaxeo}	105 °C
Max. temperature conductor, short-circuit	θ_{cmaxsc}	250 °C

Conductor shield

Thermal resistivity conductor shield	ρ_{cs}	2.5 K.m/W
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Insulation screen

Thermal resistivity insulation screen	ρ_{is}	2.5 K.m/W
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Sheath

Specific electrical resistivity sheath material	ρ_{sh}	2.840e-8 Ω .m
Temperature coefficient sheath material	α_{sh}	4.03e-3 1/K
Reciprocal of temperature coefficient sheath material	β_{sh}	2.281e2 K
Volumetric heat capacity sheath material	σ_{sh}	2.50e6 J/(K.m ³)
Thermal conductivity sheath material	k_{sh}	208.3 W/(m.K)
Density sheath material	ζ_{sh}	2.712 g/cm ³

Jacket

Thermal resistivity jacket material	ρ_j	3.5 K.m/W
Thermal resistivity additional layer	ρ_{jj}	2.5 K.m/W
Volumetric heat capacity jacket material	σ_j	2.40e6 J/(K.m ³)
Electrical conductivity jacket material	κ_j	2.00e-15 S/m
Density jacket material	ζ_j	0.941 g/cm ³

Thermal resistance**Internal thermal resistances for rating calculation**

Thermal resistance conductor—sheath $T_{ct} + T_{cs} + T_{ins} + T_{is} + T_{scb} + T_{scs} + T_{dsh}$	T_1	0.4199 K.m/W
Thermal resistance armour bedding	T_2	0 K.m/W
Thermal resistance jacket $T_{ab} + T_j + T_{jj}$	T_3	0.0542 K.m/W
Thickness conductor—sheath $t_i + t_{scb} + t_{scs} + \frac{H_{sh} + \Delta H}{2}$	t_1	18.3 mm
Thickness sheath—armour $\frac{H_{sh} + \Delta H}{2} + t_{ab}$	t_2	0 mm
Thickness armour—surface $t_j + t_{jj}$	t_3	3.5 mm

Cable elements

Thermal resistance, transient $T_1 + T_2 + T_3$	T_{tot}	0.4741 K.m/W
Thermal resistance insulation $T_{ct} + T_{cs} + T_{ins} + T_{is}$	T_i	0.41987 K.m/W
Thermal resistance conductor shield $\frac{\rho_{cs}}{2\pi} \ln \left(\frac{D_{cs}}{D_{cs} - 2t_{cs}} \right)$	T_{cs}	0.03756 K.m/W
Thermal resistance insulation $\frac{\rho_i}{2\pi} \ln \left(\frac{D_{ins}}{D_{ins} - 2t_{ins}} \right)$	T_{ins}	0.36654 K.m/W
Thermal resistance insulation screen $\frac{\rho_{is}}{2\pi} \ln \left(\frac{D_{ins} + 2t_{is}}{D_{ins}} \right)$	T_{is}	0.01577 K.m/W
Thermal resistance jacket $\frac{\rho_j}{2\pi} \ln \left(\frac{D_j - 2t_{jj}}{D_j - 2(t_j + t_{jj})} \right)$	T_j	0.0542 K.m/W

Dimensions**Diameter**

External diameter conductor	d_c	30.3 mm
Diameter over conductor shield $d_c + 2(t_{ct} + t_{cs})$	D_{cs}	33.3 mm
Diameter over insulation $d_c + 2(t_{ct} + t_{cs} + t_{ins})$	D_{ins}	64.3 mm

Diameter over insulation incl. insulation screen $d_c + 2(t_{ct} + t_{cs} + t_{ins} + t_{is})$	D_i	66.9 mm
Diameter over insulation screen $d_c + 2t_i$	D_{is}	66.9 mm
Equivalent diameter of screen and sheath	d_s	67.7 mm
Mean diameter sheath $D_{shb} + t_{sh} + H_{sh} + \Delta H$	d_{sh}	67.7 mm
Diameter over sheath $D_{shb} + 2(t_{sh} + H_{sh} + \Delta H)$	D_{sh}	68.5 mm
Diameter over sheath jacket	D_{shj}	68.5 mm
Diameter over jacket $D_{ar} + 2(t_j + t_{jj})$	D_j	75.5 mm

Area

Cross-sectional area conductor	A_c	630 mm ²
Cross-sectional area insulation $\frac{\pi}{4} (D_{is}^2 - d_c^2)$	A_i	2794.1 mm ²
Cross-sectional area sheath $d_{sh} t_{sh} \pi$	A_{sh}	170.15 mm ²
Cross-sectional area jacket $\frac{\pi}{4} (D_j^2 - (D_j - 2(t_j + t_{jj}))^2)$	A_j	791.7 mm ²