Report

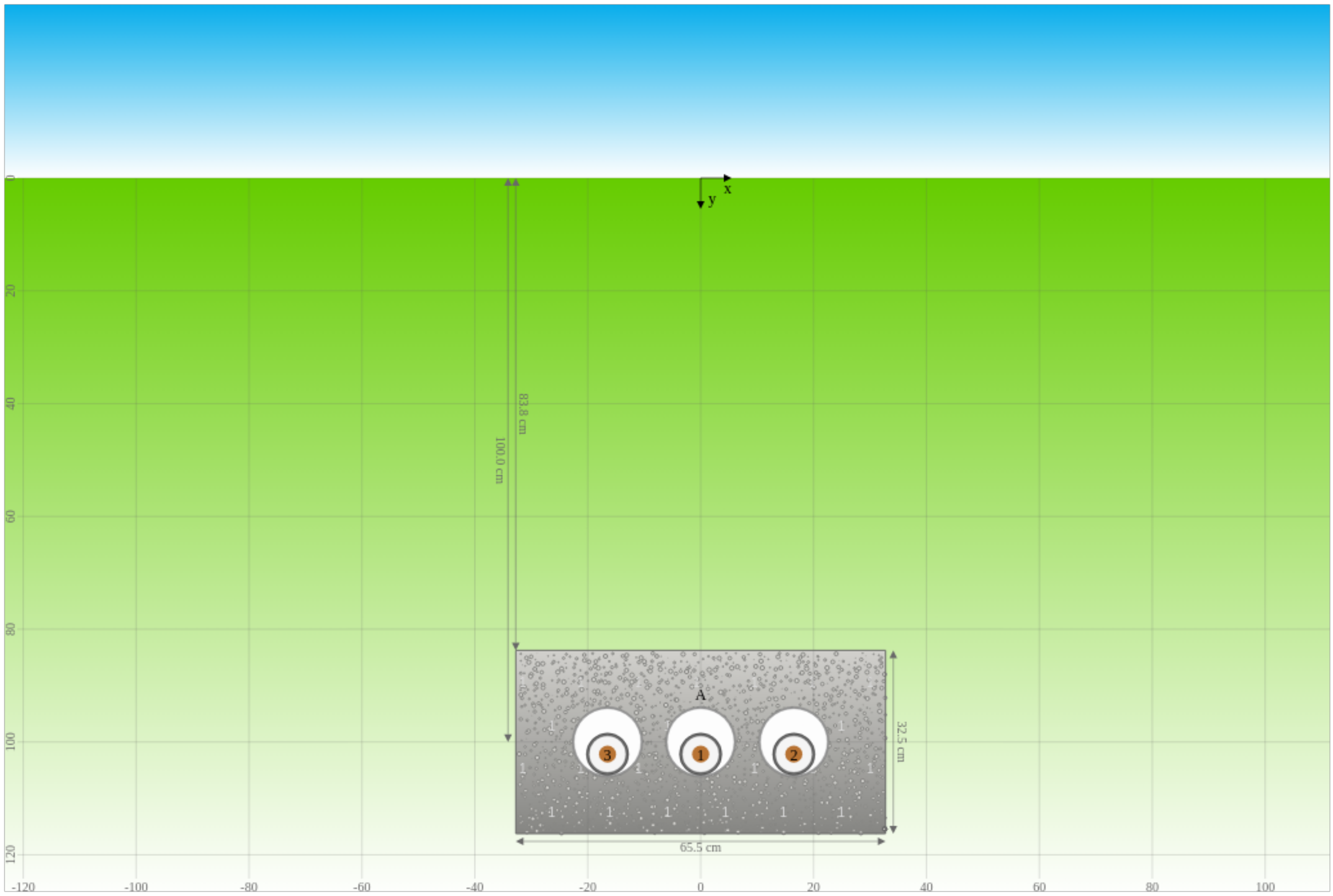
Title	Case study 0-3: Introductory (ductbank)
Project	Verification CIGRE TB 880
Created	Date: 2025-05-14 Time: 21:39 Software version: 51cac (2025-05-14)

Arrangement

Arrangement	**buried project** (#46691)
Options	None
CIGRE TB 880, guidance points	02, 06, 26, 31
Systems	A

Statistics

Number of iterations of the solver	N_{calc}	31
Sum of currents from all systems	I_{sum}	632.42 A
Sum of average conductor temperatures from all systems	θ_{sum}	85.11 °C
Number of overheated electrical systems		0
Sum of losses from all systems	W_{sum}	104.935 W/m



Systems

Following systems are active in the arrangement:

#	Object	Current [A]	Temp. [°C]	Losses [W/m]	Load
		I_c	θ_c | θ_e (θ_{de})	W_{sys}	LF
A	16173 CIGRE TB 880 Case 0 XLPE insulated ca...	632.4	90.0 | 81.2 (64.4)	104.9	1.00

Objects

Following objects are used:

16173 CIGRE TB 880 Case 0 XLPE insulated cable 132 kV

Ambient

Calculation method		IEC Standard (with backfill)
Ambient temperature	θ_a	20 °C
Thermal resistivity soil	ρ_4	1 K.m/W
Thermal conductivity soil	k_4	1 W/(m.K)
Volumetric heat capacity soil material	$c_{p,soil}$	2136.8 J/(kg.K)

$$10^{-4} \frac{{k_4}^{0.2}}{4.68}$$

Thermal diffusivity soil	δ_{soil}	5.00e-7 m^2/s
Ratio thermal resistivity dry/moist soil	v_4	1

$$\frac{\rho_{4d}}{\rho_4}$$

Constants

Standard acceleration of gravity	g	9.80665 m/s^2
Archimedes' constant π	π	3.141592653589793
Absolute temperature	θ_{abs}	273.15 K
Stefan Boltzmann constant	σ	5.67036713e-8 W/m^2K^4
Vacuum permeability	μ_0	1.2566370614359173e-6 H/m
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m

Zones

Backfill 1

Calculation method		IEC 60287-2-1 ed2.0 (2015)
Thermal resistivity backfill	ρ_b	0.8 K.m/W
Horizontal center backfill	x_b	0 mm
Vertical center backfill	L_b	1000 mm
Height backfill	h_b	325 mm
Width backfill	w_b	655 mm
Geometric factor backfill	G_b	2.185

$$\ln\left(u_b + \sqrt{{u_b}^2 - 1}\right)$$

Substitution coefficient u	u_b	4.502

$$\frac{L_b}{r_b}$$

Equivalent radius backfill	r_b	222.1 mm

$$e^{\frac{\mathrm{Min}(w_b,h_b)}{2\,\mathrm{Max}(w_b,h_b)}\left(\frac{4}{\pi}-\frac{\mathrm{Min}(w_b,h_b)}{\mathrm{Max}(w_b,h_b)}\right)\ln\left(1+\left(\frac{\mathrm{Max}(w_b,h_b)}{\mathrm{Min}(w_b,h_b)}\right)^2\right)+\ln\left(\frac{\mathrm{Min}(w_b,h_b)}{2}\right)}$$

System A (High voltage cable)

Ampacity

Cable		CIGRE TB 880 Case 0 XLPE insulated cable 132 kV
Rounded value, CIGRE TB 880	I_c	630 A
Conductor current	I_c	632.42 A

$$\sqrt{\frac{\theta_c-\theta_a+(v_4-1)\,\Delta\theta_x-v_4\Delta\theta_p-\Delta\theta_d}{R_c\left(T_1+n_{ph}\left(1+\lambda_1\right)T_2+\left(1+\lambda_1+\lambda_2+\lambda_3\right)\left(n_{ph}T_3+n_{cc}\left(T_{4i}+T_{4ii}+T_{4\mu}v_4\right)\right)+n_{cc}\lambda_4\left(\frac{T_{4ii}}{2}+T_{4\mu}v_4\right)\right)}}$$

Operating voltage	U_o	132 kV
Angular frequency	ω	314.2 rad/s

$2\pi f$

Number of sources in system	N_c	3
Number of conductors combined	n_{cc}	1

Load

System frequency	f	50 Hz
Continuous load	LF	1 p.u.

Arrangement

Duct material	M_d	duct made of plastic PVC (polyvinylchloride)
Diameter duct inner, outer	$Di_d\|Do_d$	118.6 | 125.0 mm
Thermal resistivity duct material	ρ_d	6 K.m/W
Volumetric heat capacity duct material	σ_d	1.70e6 J/(K.m^3)
Absorption coefficient solar radiation	σ_{sun}	0.6
Arrangement		flat
Position duct 1	$x_1\|y_1$	0.0 | 1000.0 mm
Position duct 2	$x_2\|y_2$	165.0 | 1000.0 mm
Position duct 3	$x_3\|y_3$	-165.0 | 1000.0 mm
Separation of conductors in a system	s_c	165 mm
Mean distance between the phases	a_m	207.89 mm
Geometric mean distance between phases of the same system	GMD	0.20789 m

$2^{\frac{1}{3}}S_m$

Depth of laying of sources	L_c	1000 mm
Depth of laying	L_{cm}	1 m
Outer diameter	D_o	0.125 m
Substitution coefficient u	u	16

$\frac{2L_{cm}}{D_o}$

Geometric constant of circle buried	g_u	31.9687

$u+\sqrt{u^2-1}$

Temperature

Temperature conductor	θ_c	1: 81.71 | 2: 83.62 | 3: 90 °C

$\theta_a+\Delta\theta_c-(v_4-1)\,\Delta\theta_x+v_4\Delta\theta_p$

Temperature screen/sheath	θ_s	1: 75.31 | 2: 77.19 | 3: 83.45 °C
Temperature sheath	θ_{sh}	1: 75.31 | 2: 77.19 | 3: 83.45 °C

$\theta_c-T_1\left(W_c+\frac{W_d}{2}\right)$

External temperature object θ_e 1: 73.81 | 2: 75.3 | 3: 81.15 °C

$$\theta_c - T_1\left(W_c + \frac{W_d}{2}\right) - n_{ph}T_2\left(W_c\left(1+\lambda_1\right)+W_d\right) - n_{ph}T_3\left(W_I + W_d\right)$$

Duct

Mean temperature medium in the duct θ_{dm} 1: 68.89 | 2: 69.14 | 3: 73.84 °C

$$\frac{\theta_e}{2} + \frac{\theta_{di}}{2}$$

Temperature duct inner surface θ_{di} 1: 63.98 | 2: 62.99 | 3: 66.53 °C

$$\theta_e - T_{4i}n_{cc}\left(W_I + W_d\right)$$

Temperature duct outer surface θ_{de} 1: 62.58 | 2: 61.24 | 3: 64.41 °C

$$\theta_{di} - T_{4ii}n_{cc}W_t + \frac{T_{4ii}W_{duct}}{2}n_{cc}$$

Temperature rise

Temperature rise conductor $\Delta\theta_c$ 1: 37.1641 | 2: 45.0037 | 3: 53.1263 K

$$n_{ph}\left(W_cT_{int} + W_dT_d\right) + n_{cc}\left(W_d\left(T_{4i} + T_{4ii} + v_4T_{4ss}\right) + \left(W_c + W_s + W_{ar} + W_{sp}\right)\left(T_{4i} + T_{4ii} + v_4T_{4\mu}\right) + W_{duct}\left(\frac{T_{4ii}}{2} + v_4T_{4\mu}\right)\right)$$

Temperature rise dielectric losses $\Delta\theta_d$ 1: 0.5077 | 2: 0.5075 | 3: 0.5042 K

$$W_d\left(n_{ph}T_d + n_{cc}\left(T_{4i} + T_{4ii} + T_{4ss}v_4\right)\right)$$

Temperature rise duct (magnetic) $\Delta\theta_{duct}$ 0 K

Temperature rise by other buried objects $\Delta\theta_p$ 1: 24.5507 | 2: 18.6211 | 3: 16.8739 K

$$\sum_{k=1}^{q}\Delta\theta_{kp}$$

Critical soil temperature rise $\Delta\theta_x$ 0 K

Losses

Ohmic

Conductor losses (phase) W_c 1: 15.058 | 2: 15.138 | 3: 15.405 W/m

$${I_c}^2R_c$$

Screen/sheath losses (phase) W_s 1: 12.31 | 2: 19.288 | 3: 26.58 W/m

$$\lambda_1W_c$$

Duct losses W_{duct} 0 W/m

Ohmic losses (phase) W_I 1: 27.368 | 2: 34.426 | 3: 41.985 W/m

$$W_c\left(1 + \lambda_1 + \lambda_2 + \lambda_3 + \lambda_4\right)$$

Dielectric

Dielectric losses (phase) W_d 0.385 W/m

$$\omega C_b\left(1000\frac{U_o}{\sqrt{3}}\right)^2\tan\delta_i$$

Total

Total losses (phase) W_t 1: 27.754 | 2: 34.811 | 3: 42.37 W/m

$$W_I + W_d$$

Total losses (object) W_{tot} 1: 27.754 | 2: 34.811 | 3: 42.37 W/m

$$n_{ph}W_t$$

Total losses (system) W_{sys} 104.935 W/m

Thermal resistance

Thermal resistance ambient $= T_{4ss} = T_{4iii} + T_{4db}$	$T_{4\mu}$	0.6498 K.m/W
Thermal resistance ambient $\frac{\rho_4}{2\pi}\left(\ln\left(g_u\right) + \ln\left(F_{mh}\right)\right)$	T_{4iii}	0.4411 K.m/W
Mutual heating coefficient	F_{mh}	1

Backfill

Thermal resistance backfill correction $\frac{N_b\left(\rho_4 - \rho_b\right)}{2\pi}G_b$	T_{4db}	0.2087 K.m/W
Number of loaded objects in backfill	N_b	3

Duct

Thermal resistance medium in the duct $\frac{U_d}{1 + 0.1\left(V_d + Y_d\theta_{dm}\right)D_{eq}}$	T_{4i}	1: 0.3542 | 2: 0.3537 | 3: 0.3451 K.m/W
Constant U for cables in ducts	U_d	1.87
Constant V for cables in ducts	V_d	0.312
Constant Y for cables in ducts	Y_d	0.0037
Thermal resistance duct wall $\frac{\rho_d}{2\pi}\ln\left(\frac{Do_d}{Di_d}\right)$	T_{4ii}	0.0502 K.m/W

Cable

Internal thermal resistance for current losses $\frac{T_1}{n_{ph}} + \left(1 + \lambda_1\right)T_2 + \left(1 + \lambda_1 + \lambda_2 + \lambda_3\right)T_3$	T_{int}	1: 0.5184 | 2: 0.5431 | 3: 0.5676 K.m/W
Internal thermal resistance for dielectric losses $\frac{T_1}{2n_c} + T_2 + T_3$	T_d	0.26414 K.m/W

Other characteristics

Earthing

earthing screen/sheath		both-side bonding
Variation of spacing		No variation

Loss factor

Loss factor shield (screen/sheath) $\lambda_{11} + F_e\lambda_{12}$	λ_1	1: 0.8175 | 2: 1.2741 | 3: 1.7254
Loss factor shield, circulating currents	λ_{11}	1: 0.7936 | 2: 1.2679 | 3: 1.7199

$$\frac{R_e}{R_c}4\xi_{X,2}$$

$$\frac{R_e}{R_c}\left(\xi_{X,3} + \xi_{X,2} - \xi_{X,1}\right)$$

$$\frac{R_e}{R_c}\left(\xi_{X,3} + \xi_{X,2} + \xi_{X,1}\right)$$

Parameter ξ calculation of loss factor | ξ_X | 1: 0.0411 | 2: 0.0366 | 3: 0.2384

$$\frac{2R_e P_X Q_X X_m}{\sqrt{3}\left(R_e{}^2 + P_X{}^2\right)\left(R_e{}^2 + Q_X{}^2\right)}$$

$$\frac{0.25 Q_X{}^2}{R_e{}^2 + Q_X{}^2}$$

$$\frac{0.75 P_X{}^2}{R_e{}^2 + P_X{}^2}$$

Loss factor shield, eddy currents | λ_{12} | 1: 0.0318 | 2: 0.0083 | 3: 0.0072

$$\frac{R_{sh}}{R_c}\left(g_s\lambda_0\left(1+\Delta_1+\Delta_2\right)+\frac{\left(\beta_1 t_{sh}\right)^4}{12{\cdot}10^{12}}\right)$$

Electrical resistance shield/armour | R_e | 1: 2.0412e-1 | 2: 2.0538e-1 | 3: 2.0959e-1 Ω/km

Substitution coefficient λ_0 for eddy-currents | λ_0 | 1: 0.0058 | 2: 0.0014 | 3: 0.0014

$$6\frac{m_0{}^2}{1+m_0{}^2}\left(\frac{d_e}{2s_c}\right)^2$$

$$1.5\frac{m_0{}^2}{1+m_0{}^2}\left(\frac{d_e}{2s_c}\right)^2$$

$$1.5\frac{m_0{}^2}{1+m_0{}^2}\left(\frac{d_e}{2s_c}\right)^2$$

Substitution coefficient Δ_1 for eddy-currents | Δ_1 | 1: 0.0006 | 2: 0.0511 | 3: -0.0493

$$0.86 m_0{}^{3.08}\left(\frac{d_e}{2s_c}\right)^{1.4m_0+0.7}$$

$$4.7 m_0{}^{0.7}\left(\frac{d_e}{2s_c}\right)^{0.16m_0+2}$$

$$\frac{-0.74\left(m_0+2\right)\sqrt{m_0}}{2+\left(m_0-0.3\right)^2}\left(\frac{d_e}{2s_c}\right)^{m_0+1}$$

Substitution coefficient Δ_2 for eddy-currents | Δ_2 | 1: 0 | 2: 0 | 3: 0

$$0$$

$$21 m_0{}^{3.3}\left(\frac{d_e}{2s_c}\right)^{1.47m_0+5.06}$$

$$0.92 m_0{}^{3.7}\left(\frac{d_e}{2s_c}\right)^{m_0+2}$$

Substitution coefficient m_0 for eddy-currents | m_0 | 1: 0.1539 | 2: 0.153 | 3: 0.1499 Hz.m/Ω

$$10^{-7}\frac{\omega}{R_{sh}}$$

Substitution coefficient β_1 for eddy-currents | β_1 | 1: 106.6166 | 2: 106.2884 | 3: 105.2147

$$\sqrt{\frac{4\pi\omega}{10^7\rho_{sh}\left(1+\alpha_{sh}\left(\theta_{sh}-20\right)\right)}}$$

Substitution coefficient g_s for eddy-currents | g_s | 1: 1.002474 | 2: 1.002464 | 3: 1.002432

$$1+\left(\frac{t_{sh}}{D_{sh}}\right)^{1.74}\left(10^{-3}\beta_1 D_{sh}-1.6\right)$$

Factor F_e eddy-current losses | F_e | 1: 0.7498 | 2: 0.752 | 3: 0.7592

$$\frac{4M_e{}^2N_e{}^2+\left(M_e+N_e\right)^2}{4\left(M_e{}^2+1\right)\left(N_e{}^2+1\right)}$$

Substitution coefficient M_e to calculate factor F_e | M_e | 1: 1.4266 | 2: 1.4354 | 3: 1.4649

$$\frac{R_e}{X_e+X_m}$$

Substitution coefficient N_e to calculate factor F_e $\frac{R_e}{X_e - \frac{X_m}{3}}$	N_e	1: 2.4011 | 2: 2.416 | 3: 2.4656
Loss factor armour	λ_2	0

Drying-out of soil

Characteristic diameter drying zone	D_{dry}	0.125 m
Depth characteristic diameter drying zone	L_{dry}	1 m
Geometric constant of circle drying zone	g_{dry}	1 p.u.
Substitution coefficient g	g_a	1

Electrical parameters

System

System length	L_{sys}	1000 m
Power factor	$\cos\varphi$	1

Resistance

Electrical resistance conductor $R_{cDC}\left(1 + y_s + y_p\right)$	R_c	1: 3.7651e-5 | 2: 3.7850e-5 | 3: 3.8517e-5 Ω/m
Electrical resistance DC conductor $R_{c20}\left(1 + \alpha_c\left(\theta_c - 20\right)\right)$	R_{cDC}	1: 3.5164e-5 | 2: 3.5376e-5 | 3: 3.6085e-5 Ω/m
Skin effect factor conductor $\frac{{x_s}^4}{192 + 0.8{x_s}^4}$	y_s	1: 0.06316 | 2: 0.06244 | 3: 0.06012
Factor for skin effect on conductor $\sqrt{10^{-7}\frac{8\pi f}{R_{cDC}}k_s}$	x_s	1: 1.89041 | 2: 1.88473 | 3: 1.86612
Proximity effect factor conductor $\frac{{x_p}^4}{192 + 0.8{x_p}^4}\left(\frac{d_c}{s_c}\right)^2\left(0.312\left(\frac{d_c}{s_c}\right)^2 + \frac{1.18}{\frac{{x_p}^4}{192+0.8{x_p}^4} + 0.27}\right)$	y_p	1: 0.00757 | 2: 0.0075 | 3: 0.00727
Factor for proximity effect of conductors $\sqrt{10^{-7}\frac{8\pi f}{R_{cDC}}k_p}$	x_p	1: 1.89041 | 2: 1.88473 | 3: 1.86612
Electrical resistance sheath $R_{sh}\left(1 + \alpha_{sh}\left(\theta_{sh} - 20\right)\right)$	R_{sh}	1: 2.0412e-4 | 2: 2.0538e-4 | 3: 2.0959e-4 Ω/m
Electrical resistance shield	R_s	1: 2.0412e-4 | 2: 2.0538e-4 | 3: 2.0959e-4 Ω/m
Reduction factor $\frac{R_s}{\sqrt{{R_s}^2 + {X_s}^2}}$	RF	1: 0.3029 | 2: 0.3046 | 3: 0.3103

Electrical field strength, capacitive load current

Electrical field strength insulation inner/outer $\frac{U_e}{1000}\frac{1}{r_x \ln\left(\frac{r_{osc}}{r_{isc}}\right)}$	E_i	6.956 | 3.603 kV/mm
Radius to point x in insulation	r_x	16.65 | 32.15 mm

Line-to-ground voltage $\frac{1000U_o}{\sqrt{3}}$	U_e	76210.24 V
Capacitance insulation $\frac{1}{2\pi\epsilon_0}\frac{10^{-9}}{18}C_b$	C_b	2.111e-10 F/m → 0.2111 μF
Capacitive load current $U_e\omega C_b$	I_C	5.054e-3 A/m → 5.0536 A
Charging capacity $n_{ph}{U_e}^2\omega C_b$	P_C	385.1382 var/m → 385.1382 kvar
Capacitive earth short-circuit current $U_e\omega C_E$	I_{Ce}	5.054e-3 A/m

Reactance

Self reactance conductor $\omega\frac{\mu_0}{2\pi}\ln\left(\frac{D_E}{GMR_c}\right)$	X_a	7.088e-4 Ω/m → 0.7088 Ω
Self reactance screen/sheath $\omega\frac{\mu_0}{2\pi}\ln\left(\frac{2s_c}{d_s}\right)$	X_e	9.953e-5 Ω/m → 0.0995 Ω
Mutual reactance between conductors flat formation without transposition $\omega\frac{\mu_0}{2\pi}\ln 2$	X_m	4.355e-5 Ω/m
Substitution coefficient P to calculate loss factor by circulating currents $X_e + X_m$	P_X	1.431e-4
Substitution coefficient Q to calculate loss factor by circulating currents $X_e - \frac{X_m}{3}$	Q_X	8.501e-5

Induced current (approximate)

Induced circulating current shield $\max\left(I_c\sqrt{\frac{\lambda_{11,sb}R_c}{R_s}}\right)$	I_s	355.545+0.000j A
Loss factor shield, circulating currents	$\lambda_{11,sb}$	1: 0.7936+0.0000j | 2: 1.2679+0.0000j | 3: 1.7199+0.0000j

Load, Voltage drop

Apparent power generator-side $\sqrt{3}U_oI_c$	S_G	144.59 MVA
Voltage drop $\sqrt{3}\left(R_c\cos\varphi + \omega L_m\sin\varphi\right)$	V_{drop}	0.065 V/(A.km) → 41.2 V = 0.03%
Inductance (mean) $\frac{\mu_0}{2\pi}\ln\left(\frac{GMD}{GMR_c}\right)$	L_m	5.750e-7+0.000e0j H/m → 0.575 mH

Telegrapher equation

Surge impedance $\sqrt{\frac{Z_1}{Y_1}}$	Z_C	1: 52.4744-5.4101j | 2: 52.4774-5.4385j | 3: 52.4873-5.5333j Ω
Propagation constant $\sqrt{Z_1 Y_1}$	γ_C	1: 3.588e-7+3.480e-6j | 2: 3.606e-7+3.480e-6j | 3: 3.669e-7+3.481e-6j

Impedance valid up to 100 Hz without earth return

Positive sequence admittance $G + j\omega C_b$	Y_1	0.000e0+6.631e-8j S/m → 0.0000+0.0001j S
Positive sequence impedance $R_1 + jX_1$	Z_1	1: 3.765e-5+1.807e-4j | 2: 3.785e-5+1.807e-4j | 3: 3.852e-5+1.807e-4j Ω/m
Positive sequence reactance $\omega \frac{\mu_0}{2\pi} \ln\left(\frac{GMD}{GMR_c}\right)$	X_1	1.807e-4 Ω/m → 0.1807 Ω

Cable datasheet

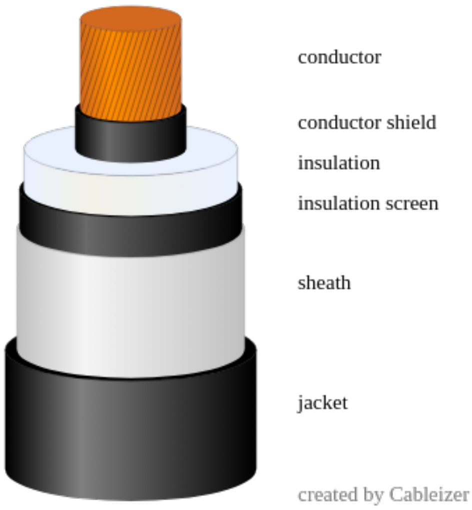
Title	CIGRE TB 880 Case 0 XLPE insulated cable 132 kV (#16173)

Cable is used in following systems: A

CIGRE TB 880, guidance points	15, 20, 23, 25, 30, 32, 33, 34, 38, 39, 42, 44, 45

General Data

Rated line-to-line voltage	U_n	132 kV
Base voltage for tests	U_0	76 kV
Highest voltage for equipment	U_m	145 kV
Nominal system frequency	f	50 Hz
Number of conductors cable	n_c	1
Number of phases in a cable	n_{ph}	1



Cable elements

Conductor

Cross-sectional area conductor	A_c	1 x 630 mm^2
Conductor material	M_c	Copper, round stranded
External diameter conductor	d_c	30.3 mm
Radius conductor	r_c	15.15 mm

$$\frac{d_c}{2}$$

Insulation

Insulation material	M_i	Crosslinked polyethylene (XLPE)
Thickness conductor shield	t_{cs}	1.5 mm
Thickness insulation	t_{ins}	15.5 mm
Thickness insulation screen	t_{is}	1.3 mm
Thickness insulation	t_i	18.3 mm

$$t_{ct} + t_{cs} + t_{ins} + t_{is}$$

Sheath

Sheath material	M_{sh}	Aluminium
Thickness sheath	t_{sh}	0.8 mm
corrugated		No

Jacket

Jacket material	M_j	High density polyethylene (HDPE, ST7)
Thickness jacket	t_j	3.5 mm

Overall

External diameter object	D_e	75.5 mm
Absorption coefficient solar radiation	σ_{sun}	0.4
Emissivity cable	ϵ_e	0.9
Reflectivity cable $1-\epsilon_e$	η_e	0.1
Mass cable $m_{hollow}+m_{metal}$	m_{tot}	9.418 kg/m

Electrical

Conductor

Electrical resistance DC conductor 20°C	R_{c20}	2.8300e-5 Ω/m
Standard DC resistance of conductor	R_{co}	0.0283 Ω/km
Coating of wires		plain
Skin effect coefficient	k_s	1
Proximity effect coefficient	k_p	1
Geometric mean radius conductor $K_{GMR}r_{z1}$	GMR_c	0.01173 m
Factor geometric mean radius	K_{GMR}	0.774
Constant relating to conductor formation	K_{BICC}	0.0512
Number of wires conductor	n_{cw}	91
Diameter of wires conductor (average)	d_{cw}	2.97 mm

Insulation

Capacitance, with approximation (CIGRE TB 880) $\frac{1}{2\pi\epsilon_0}\frac{10^{-9}}{18}C_b$	C_b	2.111e-10 F/m
Capacitance (exact) $\frac{2\pi\epsilon_0\epsilon_i}{\ln\left(\frac{r_{osc}}{r_{isc}}\right)}$	C_b	2.114e-10 F/m
Capacitance to earth C_b	C_E	2.111e-10 F/m
Vacuum permittivity	ϵ_0	8.854187817620389e-12 F/m
Radius above the inner semi-conducting layer $\frac{d_c}{2}+t_{ct}+t_{cs}$	r_{isc}	16.65 mm
Radius over capacitive insulation layers $\frac{D_{ins}}{2}$	r_{osc}	32.15 mm

Velocity of propagation $\frac{1}{1000\sqrt{\mu_0 \epsilon_0 \epsilon_i}}$	v_{prop}	189605.4 km/s

Screen + Sheath

Electrical resistance sheath $10^6 \frac{\rho_{sh}}{A_{sh}}$	R_{sh}	1.6691e-4 Ω/m
Electrical resistance screen/sheath 20°C	R_{so}	1.669e-1 Ω/km

Radius

Radius conductor	r_{z1}	0.01515 m
Radius shield (inner)	r_{z2}	0.03305 m
Radius shield (outer)	r_{z3}	0.03305 m
Radius sheath (inner)	$r_{z2,sh}$	0.03305 m
Radius sheath (outer)	$r_{z3,sh}$	0.03465 m
Radius outersheath	r_{z6}	0.03775 m

Material parameters

Conductor

Electrical resistivity conductor material	ρ_c	1.724e-8 Ω.m
Temperature coefficient conductor material	α_c	3.93e-3 1/K
Reciprocal of temperature coefficient conductor material	β_c	2.345e2 K
Volumetric heat capacity conductor material	σ_c	3.45e6 J/(K.m^3)
Thermal conductivity conductor material	k_c	384.62 W/(m.K)
Density conductor material	ζ_c	8.94 g/cm^3

Insulation

Relative permittivity insulation material	ϵ_i	2.5
Loss factor insulation material	$\tan\delta_i$	0.001
Thermal resistivity insulation material	ρ_i	3.5 K.m/W
Volumetric heat capacity insulation material	σ_i	2.40e6 J/(K.m^3)
Density insulation material	ζ_i	0.923 g/cm^3
Max. temperature conductor	θ_{cmax}	90 °C
Max. temperature conductor, emergency overload	θ_{cmaxeo}	105 °C
Max. temperature conductor, short-circuit	θ_{cmaxsc}	250 °C
Conductor shield		
Thermal resistivity conductor shield	ρ_{cs}	2.5 K.m/W
Insulation screen		
Thermal resistivity insulation screen	ρ_{is}	2.5 K.m/W

Sheath

Specific electrical resistivity sheath material	ρ_{sh}	2.840e-8 Ω.m
Temperature coefficient sheath material	α_{sh}	4.03e-3 1/K
Reciprocal of temperature coefficient sheath material	β_{sh}	2.281e2 K
Volumetric heat capacity sheath material	σ_{sh}	2.50e6 J/(K.m^3)
Thermal conductivity sheath material	k_{sh}	208.3 W/(m.K)
Density sheath material	ζ_{sh}	2.712 g/cm^3

Jacket

Thermal resistivity jacket material	ρ_j	3.5 K.m/W
Thermal resistivity additional layer	ρ_{jj}	2.5 K.m/W
Volumetric heat capacity jacket material	σ_j	2.40e6 J/(K.m^3)
Electrical conductivity jacket material	κ_j	2.00e-15 S/m
Density jacket material	ζ_j	0.941 g/cm^3

Thermal resistance

Internal thermal resistances for rating calculation

Thermal resistance conductor—sheath — T_1 — 0.4199 K.m/W

$$T_{ct} + T_{cs} + T_{ins} + T_{is} + T_{scb} + T_{scs} + T_{dsh}$$

Thermal resistance armour bedding — T_2 — 0 K.m/W

Thermal resistance jacket — T_3 — 0.0542 K.m/W

$$T_{ab} + T_j + T_{jj}$$

Thickness conductor—sheath — t_1 — 18.3 mm

$$t_i + t_{scb} + t_{scs} + \frac{H_{sh} + \Delta H}{2}$$

Thickness sheath—armour — t_2 — 0 mm

$$\frac{H_{sh} + \Delta H}{2} + t_{ab}$$

Thickness armour—surface — t_3 — 3.5 mm

$$t_j + t_{jj}$$

Cable elements

Thermal resistance, transient — T_{tot} — 0.4741 K.m/W

$$T_1 + T_2 + T_3$$

Thermal resistance insulation — T_i — 0.41987 K.m/W

$$T_{ct} + T_{cs} + T_{ins} + T_{is}$$

Thermal resistance conductor shield — T_{cs} — 0.03756 K.m/W

$$\frac{\rho_{cs}}{2\pi} \ln\left(\frac{D_{cs}}{D_{cs} - 2t_{cs}}\right)$$

Thermal resistance insulation — T_{ins} — 0.36654 K.m/W

$$\frac{\rho_i}{2\pi} \ln\left(\frac{D_{ins}}{D_{ins} - 2t_{ins}}\right)$$

Thermal resistance insulation screen — T_{is} — 0.01577 K.m/W

$$\frac{\rho_{is}}{2\pi} \ln\left(\frac{D_{ins} + 2t_{is}}{D_{ins}}\right)$$

Thermal resistance jacket — T_j — 0.0542 K.m/W

$$\frac{\rho_j}{2\pi} \ln\left(\frac{D_j - 2t_{jj}}{D_j - 2\left(t_j + t_{jj}\right)}\right)$$

Dimensions

Diameter

External diameter conductor — d_c — 30.3 mm

Diameter over conductor shield — D_{cs} — 33.3 mm

$$d_c + 2\left(t_{ct} + t_{cs}\right)$$

Diameter over insulation — D_{ins} — 64.3 mm

$$d_c + 2\left(t_{ct} + t_{cs} + t_{ins}\right)$$

Diameter over insulation incl. insulation screen $d_c + 2\left(t_{ct} + t_{cs} + t_{ins} + t_{is}\right)$	D_i	66.9 mm
Diameter over insulation screen $d_c + 2t_i$	D_{is}	66.9 mm
Equivalent diameter of screen and sheath	d_s	67.7 mm
Mean diameter sheath $D_{shb} + t_{sh} + H_{sh} + \Delta H$	d_{sh}	67.7 mm
Diameter over sheath $D_{shb} + 2\left(t_{sh} + H_{sh} + \Delta H\right)$	D_{sh}	68.5 mm
Diameter over sheath jacket	D_{shj}	68.5 mm
Diameter over jacket $D_{ar} + 2\left(t_j + t_{jj}\right)$	D_j	75.5 mm

Area

Cross-sectional area conductor	A_c	630 mm^2
Cross-sectional area insulation $\frac{\pi}{4}\left({D_{is}}^2 - {d_c}^2\right)$	A_i	2794.1 mm^2
Cross-sectional area sheath $d_{sh} t_{sh} \pi$	A_{sh}	170.15 mm^2
Cross-sectional area jacket $\frac{\pi}{4}\left({D_j}^2 - \left(D_j - 2\left(t_j + t_{jj}\right)\right)^2\right)$	A_j	791.7 mm^2